

Q1. (a) Prove from first principles that two capacitors C_1 and C_2 connected in series can be replaced with an equivalent capacitance of $C_1 C_2 / (C_1 + C_2)$. [2 marks]

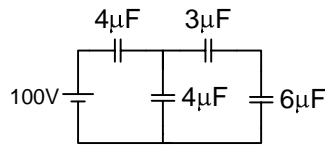


Figure Q1-(b)

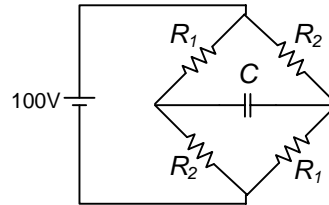


Figure Q1-(c)

(b) Find the voltage across each capacitor of the circuit in Figure Q1-(b). [4 marks]

(c) Find an expression for the charging time constant of the capacitor C shown in Figure Q1-(c). Also find the steady state voltage across the capacitor. [4 marks]

ANSWER

(a) Let Q_1 be the charge on C_1 and Q_2 charge on C_2 , then $Q_1 = C_1 V_1$ and $Q_2 = C_2 V_2$.

For the equivalent capacitor C , we have $Q = CV$

Since the two capacitors are in series,

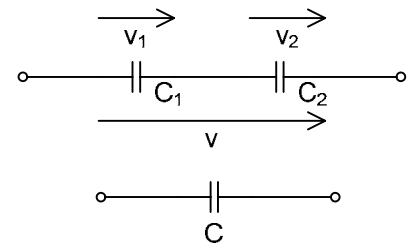
$Q_1 = Q_2 = Q$, Hence we have,

$$V = V_1 + V_2 = \frac{Q}{C_1} + \frac{Q}{C_2} = Q \cdot \left[\frac{1}{C_1} + \frac{1}{C_2} \right],$$

Comparing with $Q = CV$, we get

$$\frac{1}{C} = \frac{1}{C_1} + \frac{1}{C_2} \text{ or}$$

$$C = \frac{C_1 C_2}{C_1 + C_2}$$



(b) The equivalent circuits are given below,

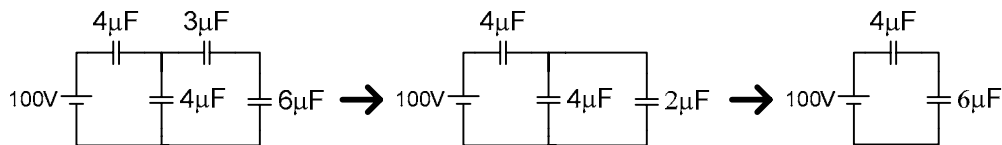
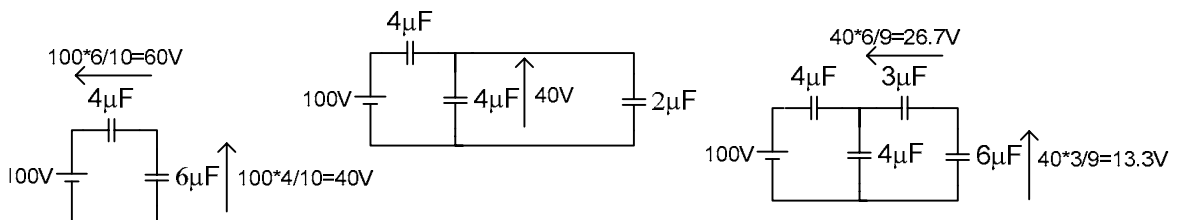


Figure Q1-(b)

Using the voltage division rule, we get the following



(c) Get the Thevenin's equivalent across the capacitor.

$$R_{th} = (R_1 // R_2) + (R_1 // R_2), \text{ therefore, } R_{th} = 2 \cdot R_1 \cdot R_2 / (R_1 + R_2)$$

Also,

$$E_{th} = E \left(\frac{R_2}{R_1 + R_2} - \frac{R_1}{R_1 + R_2} \right) = E \left(\frac{R_2 - R_1}{R_1 + R_2} \right)$$

Hence,

$$\text{The time constant} = R_{th} \cdot C = 2 \cdot R_1 \cdot R_2 \cdot C / (R_1 + R_2)$$

$$\text{Final Voltage} = E_{th} = 100 \cdot \left(\frac{R_2 - R_1}{R_1 + R_2} \right)$$

Q2. (a) Write a differential equation relating output current $i(t)$ to the input voltage $v(t)$ for the circuit in Figure Q2. [5 marks]

(b) By means of the differential equation derived above, answer the following.

i. What is the order of the differential equation? How is the order of the differential equation related to the circuit in question? [1 mark]

ii. If the input voltage $v(t)$ is a DC source of magnitude E , what is the current at steady state? [1 mark]

iii. If the input voltage $v(t)$ is an AC source of angular frequency ω , derive an expression for the input impedance of the circuit. [2 marks]

iv. Validate your answer in part (iii) above using AC theory. [1 mark]

ANSWER

(a) We can write the following equations for V_1 , V_2 and V .

$$V = V_1 + V_2 \dots\dots\dots (1)$$

$$i = i_1 + i_2 \dots\dots\dots (2)$$

$$V_1 = L_1 \frac{di_2}{dt} \dots\dots\dots (3)$$

$$V_1 = \frac{1}{C_1} \int i_1 dt \dots\dots\dots (4)$$

$$V_2 = iR_2 + L_2 \frac{di}{dt} \dots\dots\dots (5)$$

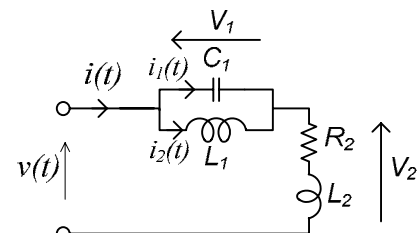


Figure Q2

Differentiating equation (4) twice yields $\frac{di_1}{dt} = C_1 \frac{d^2V_1}{dt^2}$, and combining with equation (3),

we get, $\frac{di}{dt} = \frac{di_1}{dt} + \frac{di_2}{dt} = C_1 \frac{d^2V_1}{dt^2} + \frac{V_1}{L_1}$, or $\frac{1}{C_1} \frac{di}{dt} = \frac{d^2V_1}{dt^2} + \frac{V_1}{L_1C_1} \dots\dots\dots (6)$

Also, differentiating equation (5) twice yields $R_2 \frac{d^2i}{dt^2} + L_2 \frac{d^3i}{dt^3} = \frac{d^2V_2}{dt^2} \dots\dots\dots (7)$

Adding (6) and (7),

$$\frac{1}{C_1} \frac{di}{dt} + R_2 \frac{d^2i}{dt^2} + L_2 \frac{d^3i}{dt^3} = \frac{d^2V_1}{dt^2} + \frac{V_1}{L_1C_1} + \frac{d^2V_2}{dt^2} \dots\dots\dots (8)$$

Substituting from equation (1) and its derivatives, (8) becomes

$$\begin{aligned}\frac{1}{C_1} \frac{di}{dt} + R_2 \frac{d^2i}{dt^2} + L_2 \frac{d^3i}{dt^3} &= \frac{d^2V}{dt^2} + \frac{1}{L_1 C_1} (V - V_2) \\ &= \frac{d^2V}{dt^2} + \frac{1}{L_1 C_1} \left(V - iR_2 - L_2 \frac{di}{dt} \right)\end{aligned}$$

Re-arranging the terms,

$$\boxed{\frac{d^3i}{dt^3} + \frac{R_2}{L_2} \cdot \frac{d^2i}{dt^2} + \frac{1}{C_1} \left(\frac{1}{L_1} + \frac{1}{L_2} \right) \frac{di}{dt} + \frac{R_2}{L_1 L_2 C_1} i = \frac{1}{L_2} \cdot \frac{d^2V}{dt^2} + \frac{1}{L_1 L_2 C_1} \cdot V}$$

(b) Using the above differential equation,

- i. The order of the differential equation is 3. This is because the circuit has 3 independent energy storing elements.
- ii. To find steady state current, substitute $di/dt=0$ and $dV/dt=0$ (all higher derivatives are also zero). Thus, $I = E/R_2$.
- iii. Substitute $d/dt = j\omega$, (and swapping left and right hand sides)

$$\left[\frac{1}{L_2} \cdot (j\omega)^2 + \frac{1}{L_1 L_2 C_1} \right] \cdot V = \left[(j\omega)^3 + \frac{R_2}{L_2} \cdot (j\omega)^2 + \frac{1}{C_1} \left(\frac{1}{L_1} + \frac{1}{L_2} \right) (j\omega) + \frac{R_2}{L_1 L_2 C_1} \right] \cdot I$$

$$\left[-\frac{1}{L_2} \omega^2 + \frac{1}{L_1 L_2 C_1} \right] \cdot V = \left[-j\omega^3 - \frac{R_2}{L_2} \cdot \omega^2 + j \frac{1}{C_1} \left(\frac{1}{L_1} + \frac{1}{L_2} \right) \omega + \frac{R_2}{L_1 L_2 C_1} \right] \cdot I$$

$$\frac{(1 - \omega^2 L_1 C_1)}{L_1 L_2 C_1} \cdot V = \frac{[-j\omega^3 L_1 L_2 C_1 - R_2 L_1 C_1 \omega^2 + j(L_1 + L_2)\omega + R_2]}{L_1 L_2 C_1} \cdot I$$

$$\frac{V}{I} = \frac{R_2(1 - \omega^2 L_1 C_1) + j\omega(L_1 + L_2 - \omega^2 L_1 L_2 C_1)}{(1 - \omega^2 L_1 C_1)}$$

$$= R_2 + j\omega L_2 + \frac{j\omega L_1}{(1 - \omega^2 L_1 C_1)}$$

iv. Using AC theory, the impedance is

$$Z = R_2 + j\omega L_2 + \frac{j\omega L_1 \cdot \frac{1}{j\omega C_1}}{j\omega L_1 + \frac{1}{j\omega C_1}}$$

$$= R_2 + j\omega L_2 + \frac{j\omega L_1}{(1 - \omega^2 L_1 C_1)}$$

Q3. (a) Derive an expression for the total energy stored in the coupled circuit in Figure Q3-(a). [2 marks]

(b) The circuit in Figure Q3-(b) is supplied by a sinusoidal voltage source V_s of variable frequency. The output V_{out} is taken across the inductor.

i. Write an expression for the output voltage V_{out} as a function of the input voltage V_s . [1 mark]

ii. Find an expression for the resonance frequency of the circuit. [1]

iii. Show that half-power frequencies are given by, [2 marks]

$$f_1, f_2 = \pm \frac{1}{4\pi RC} + \frac{1}{2\pi} \sqrt{\frac{1}{(2RC)^2} + \frac{1}{LC}}$$

iv. If the circuit is to be designed with a resonance frequency of 3.2 kHz and a bandwidth of 1 kHz, calculate the appropriate values for L and C , given that $R = 2.0 \text{ k}\Omega$. [2 marks]

v. With the circuit parameters as found in part (iv) above, determine the output voltage at the frequencies of f_1 and f_2 , when $V_s = 10\text{V}$. [2 marks]

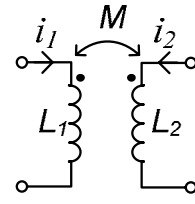


Figure Q3-(a)

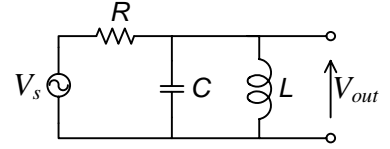


Figure Q3-(b)

ANSWER

(a) Total energy stored

$$\begin{aligned} W &= \int v_1 i_1 dt + \int v_2 i_2 dt \\ &= \int \left(L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \right) i_1 dt + \int \left(L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \right) i_2 dt \\ &= \int L_1 i_1 di_1 + \int L_2 i_2 di_2 + M \int (i_1 di_2 + i_2 di_1) \\ &= \frac{1}{2} L_1 i_1^2 + \frac{1}{2} L_2 i_2^2 + M i_1 i_2 \end{aligned}$$

(b) (i). The output voltage is given by,

$$\begin{aligned} V_{out} &= \frac{Z}{R+Z} \cdot V_s, \text{ where } Z \text{ is the impedance of } L \text{ and } C \text{ in parallel.} \\ &= \frac{\frac{j\omega L}{1-\omega^2 LC}}{R + \frac{j\omega L}{1-\omega^2 LC}} \cdot V_s \\ &= \left(\frac{j\omega L}{R(1-\omega^2 LC) + j\omega L} \right) \cdot V_s \\ &= \left[\frac{1}{1 - j \frac{R}{\omega L} (1 - \omega^2 LC)} \right] \cdot V_s \end{aligned}$$

(ii). The resonance frequencies are given by unity power factor,

$$\begin{aligned} \frac{R}{\omega L} (1 - \omega^2 LC) &= 0 \\ \omega_0 &= \sqrt{\frac{1}{LC}} \end{aligned}$$

(iii). At half-power frequencies,

$$\left[\frac{1}{1 - j \frac{R}{\omega L} (1 - \omega^2 LC)} \right] \cdot V_s = \frac{V_s}{\sqrt{2}}, \text{ Since at resonance the output voltage is } V_s$$

$$\text{i.e., } \frac{R}{\omega L} (1 - \omega^2 LC) = \pm 1$$

Taking the positive sign,

$$R - \omega^2 RLC = \omega L$$

$$\omega^2 + \left(\frac{1}{RC} \right) \omega - \left(\frac{1}{LC} \right) = 0$$

$$\omega_1 = -\frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC} \right)^2 + \frac{1}{LC}}, \text{ Note that the other solution yields a negative frequency and hence it is ignored.}$$

Taking the negative sign,

$$\omega^2 - \left(\frac{1}{RC} \right) \omega - \left(\frac{1}{LC} \right) = 0$$

$$\omega_2 = \frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC} \right)^2 + \frac{1}{LC}}, \text{ Note that the other solution yields a negative frequency and hence it is ignored.}$$

$$f_1, f_2 = \pm \frac{1}{4\pi RC} + \frac{1}{2\pi} \sqrt{\left(\frac{1}{2RC} \right)^2 + \frac{1}{LC}}$$

(iv). Resonance frequency,

$$f_0 = \frac{1}{2\pi} \sqrt{\frac{1}{LC}} = 3200 \text{ Hz}$$

$$LC = \frac{1}{4\pi^2 f_0^2} = 2.474 \times 10^{-9}$$

Bandwidth is given by,

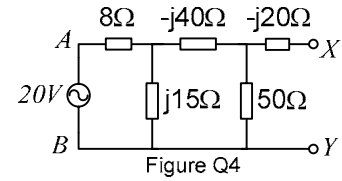
$$f_1 - f_2 = 2 \times \frac{1}{4\pi RC} = 1000 \text{ Hz}$$

$$RC = \frac{1}{2\pi(\text{BW})} = 1.592 \times 10^{-4}$$

Therefore, $C = 0.08 \mu\text{F}$ and $L = 31 \text{ mH}$.

(v). The output voltage at half-power frequencies must be $1/\sqrt{2}$ of peak output at resonance. Since the peak output is 10V, the output at half-power frequencies is 7.07V.

- Q4.** (a) For the circuit in Figure Q4, find the input impedance across XY . [2 marks]
 (b) Find the short circuit current through XY . [2 marks]
 (c) Find the Norton's equivalent circuit across XY . [2 marks]
 (d) If the voltage source is moved to the terminals XY , What would be the Norton's equivalent circuit across AB ? [2 marks]
 (e) Are the two Norton's equivalent circuits identical? Comment on your results. [2 marks]



ANSWER

- (a) The impedance across XY , is Z_{XY} .

$$Z_1 = 8 \parallel j15 = 6.2284 + j3.3218$$

$$Z_2 = Z_1 - j40 = 6.2284 - j36.6782$$

$$Z_3 = Z_2 \parallel 50 = 18.8100 - j20.3455$$

$$Z_{XY} = Z_3 - j20 = 18.8100 - j40.3455$$

$$Y_{XY} = \frac{1}{Z_{XY}} = 0.0095 + j0.0204$$

- (b) First, find the total impedance when XY are short circuited.

$$Z_4 = -j20 \parallel 50 = 6.8966 - j17.2414$$

$$Z_5 = Z_4 - j40 = 6.8966 - j57.2414$$

$$Z_6 = Z_5 \parallel j15 = 0.8471 + j20.1882$$

$$Z_{sc} = Z_6 + 8 = 8.8471 + j20.1882$$

$$\therefore I_1 = \frac{20}{8.8471 + j20.1882} = 0.3642 - j0.8311, \text{ this is the s/c current at the source.}$$

Using current division rule successively,

$$I_2 = \frac{j15}{Z_5 + j15} I_1 = -0.0790 + j0.3080$$

$$I_{sc} = \frac{50}{50 - j20} I_2 = -0.1744 + j0.2383$$

- (c) Hence, the Norton equivalent circuit has a current source of $(-0.1744 + j0.2383)$ A and a parallel admittance of $Y_{XY} = 0.0095 + j0.0204$
 (d) When the voltage source is moved to XY , using the reciprocity theorem, the short circuit current across AB must be the same as the short circuit current I_{sc} found earlier.
 By inspection, the input impedance across AB , must be the same as Z_{sc} calculated in part (b) above.
 (e) The two equivalent circuits are not identical. However, they have the same current source but different admittances in parallel.

- Q5.** (a) An alternating voltage source V_s has an internal impedance of $r + jx$. Find an expression for the purely resistive load R_p which when connected to the source, maximises the real output power. [4 marks]
- (b) Derive an expression for the source efficiency for the above circuit when it delivers maximum power. [3 marks]
- (c) You need to design a 10V, AC source such that for purely resistive loads, it delivers a maximum of 12.5W at a source efficiency of 75 percent. Determine the internal impedance of the source. [3 marks]

ANSWER

- (a) When a purely resistive load R is connected, the power output is given by

$$P = I^2 R = \left| \frac{V}{r + jx + R} \right|^2 \cdot R$$

$$= \frac{V^2}{(R + r)^2 + x^2} \cdot R$$

For maximum power, $dP/dR = 0$

$$\frac{dP}{dR} = V^2 \cdot R(2(r + R)) - V^2 \cdot [(r + R)^2 + x^2] \cdot 1 = 0$$

$$2R(r + R) = (r + R)^2 + x^2$$

$$R^2 = r^2 + x^2$$

$$\therefore R_p = \sqrt{r^2 + x^2}$$

- (b) The source efficiency at maximum power,

$$\eta = \frac{\text{Output Power}}{\text{Total Power at source}} = \frac{|I_m|^2 R_p}{|I_m|^2 (R_p + r)} = \frac{\sqrt{r^2 + x^2}}{r + \sqrt{r^2 + x^2}}$$

$$= \frac{\sqrt{1 + (x/r)^2}}{1 + \sqrt{1 + (x/r)^2}}$$

- (c) The maximum power delivered to the load,

$$P_L = |I_m|^2 R_p$$

$$= \frac{V^2}{(r + \sqrt{r^2 + x^2})^2 + x^2} \cdot \sqrt{r^2 + x^2}$$

$$= \frac{V^2}{2(r^2 + x^2) + 2r\sqrt{r^2 + x^2}} \cdot \sqrt{r^2 + x^2}$$

$$= \frac{V^2}{2r} \cdot \left[\frac{\sqrt{1 + (x/r)^2}}{1 + (x/r)^2 + \sqrt{1 + (x/r)^2}} \right]$$

From the equation for efficiency, $\eta = 0.75$, we get $(x/r)^2 = 8$ or $x/r = 2.828$.

By substituting for x/r in equation for P_L , we get, $r = 1.0\Omega$. Hence, $x = 2.828\Omega$.

Q6. (a) Find the ABCD parameters for the transformer circuit in Figure Q6-(a). [5 marks]

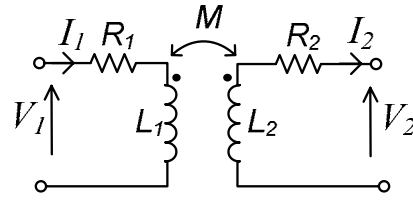


Figure Q6-(a)

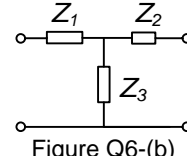


Figure Q6-(b)

(b) Find appropriate values for Z_1 , Z_2 and Z_3 of the T-network in Figure Q6-(b) such that it is equivalent to the transformer circuit in Figure Q6-(a). [5 marks]

ANSWER

(a) Writing the Kirchhoff's law for the two loops,

$$V_1 = I_1 R_1 + j\omega L_1 I_1 - j\omega M I_2$$

$$V_2 = I_2 R_2 - j\omega L_2 I_2 + j\omega M I_1$$

Using the above equations together with the definitions for A, B, C and D,

$$A = \left. \frac{V_1}{V_2} \right|_{I_2=0} = \frac{R_1 I_1 + j\omega L_1 I_1}{j\omega M I_1} = \frac{R_1 + j\omega L_1}{j\omega M}$$

$$B = \left. \frac{V_1}{I_2} \right|_{V_2=0} = \frac{I_1 R_1 + j\omega L_1 I_1 - j\omega M I_2}{I_2} = (R_1 + j\omega L_1) \frac{I_1}{I_2} - j\omega M$$

But from second equation above, $\frac{I_1}{I_2} = \frac{(R_2 + j\omega L_2)}{j\omega M}$

$$\therefore B = (R_1 + j\omega L_1) \frac{(R_2 + j\omega L_2)}{j\omega M} - j\omega M = \frac{1}{j\omega M} [(R_1 + j\omega L_1)(R_2 + j\omega L_2) - \omega^2 M^2]$$

$$C = \left. \frac{I_1}{V_2} \right|_{I_2=0} = \frac{I_1}{j\omega M I_1} = \frac{1}{j\omega M}$$

$$D = \left. \frac{I_1}{I_2} \right|_{V_2=0} = \frac{(R_2 + j\omega L_2)}{j\omega M}$$

(b) For the T-network,

$$\begin{aligned} \begin{bmatrix} A & B \\ C & D \end{bmatrix} &= \begin{bmatrix} 1 & Z_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ Y_3 & 1 \end{bmatrix} \begin{bmatrix} 1 & Z_2 \\ 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} (1+Z_1 Y_3) & Z_2 + (1+Z_2 Y_3) Z_1 \\ Y_3 & (1+Z_2 Y_3) \end{bmatrix} \end{aligned}$$

By comparing the two sets of parameters,

For parameter C,

$$Y_3 = \frac{1}{j\omega M} \text{ which yields } Z_3 = j\omega M$$

For parameter A,

$$(1 + Z_1 Y_3) = \frac{R_1 + j\omega L_1}{j\omega M}$$

Substituting for Y_3 , $Z_1 = R_1 + j\omega L_1 - j\omega M = R_1 + j\omega(L_1 - M)$

Similarly for parameter C,

$$(1 + Z_2 Y_3) = \frac{R_2 + j\omega L_2}{j\omega M}$$

Substituting for Y_3 , $Z_2 = R_2 + j\omega L_2 - j\omega M = R_2 + j\omega(L_2 - M)$

- Q7. (a)** Using the first principles and general properties of Laplace transform, find the Laplace transform of causal time function $f(t) = e^{-at} \sin \omega t$. [2 marks]

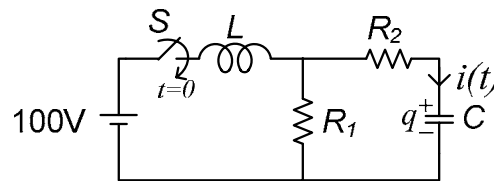


Figure Q7

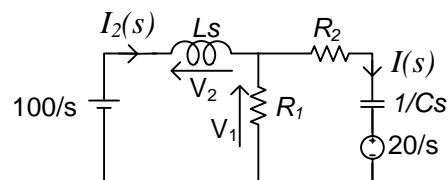
- (b)** In the circuit of Figure Q7, the capacitor has an initial charge of $500\mu\text{C}$. If the switch S is closed at $t = 0$, using Laplace transform method, find an expression in time t for the subsequent variation of current $i(t)$. [5 marks]
- (c)** If $L=1 \text{ mH}$, $R_1=400\Omega$, $R_2=600\Omega$ and $C=25\mu\text{F}$, determine the following values related to $i(t)$, [2 marks]
- iv.** initial current,
 - v.** time at which current becomes zero momentarily,
 - vi.** peak value of current and the time it occurs,
 - vii.** steady state value of current.
- (d)** Sketch, approximately to scale, the current wave form $i(t)$ from $t = 0$ to 100ms. [1 mark]

ANSWER

- (a)** See class notes for the Laplace transform of $\sin \omega t$. Multiplying by e^{-at} in time domain will have the effect of shifting $s \rightarrow (s+a)$ in frequency domain. Combining these two results, we

$$\text{get } F(s) = \frac{\omega}{(s+a)^2 + \omega^2}.$$

- (b)** When converted to frequency domain the circuit becomes (the initial charge is equal to 20V step input in series with the capacitor),



And applying Kirchhoff's law's,

$$V_1 = R_2 I(s) + \frac{1}{Cs} I(s) + \frac{20}{s} \dots\dots\dots (1)$$

$$\frac{100}{s} = V_1 + V_2 \dots\dots\dots (2)$$

Equation (2) yields,

$$\frac{100}{s} = V_1 + Ls \cdot I_2(s)$$

$$= V_1 + Ls \cdot \left(I(s) + \frac{V_1}{R_1} \right)$$

$$= V_1 \left(1 + \frac{Ls}{R_1} \right) + Ls \cdot I(s)$$

Substituting for V_1 from (1),

$$= \left(R_2 I(s) + \frac{1}{Cs} I(s) + \frac{20}{s} \right) \cdot \left(1 + \frac{Ls}{R_1} \right) + Ls \cdot I(s)$$

$$= \left[\left(R_2 + \frac{1}{Cs} \right) \left(1 + \frac{Ls}{R_1} \right) + Ls \right] \cdot I(s) + \frac{20}{s} + \frac{20L}{R_1}$$

Solving for $I(s)$,

$$I(s) = \frac{80 - 20 \left(\frac{L}{R_1} \right) s}{L \left(\frac{R_1 + R_2}{R_1} \right) s^2 + \left(\frac{L + R_1 R_2 C}{R_1 C} \right) s + \frac{1}{C}}$$

The above expression has a second order denominator and a first order numerator.

In general this expression can be factored as,

$$I(s) = k \cdot \frac{a - b}{(s + a)(s + b)}$$

Hence the time domain expression for current $i(t)$ is,

$$i(t) = k_1 \cdot e^{-at} - k_2 \cdot e^{-bt}$$

(c) Substituting values,

$$I(s) = \frac{80 - 5 \times 10^{-5} s}{0.0025 s^2 + 600 s + 40000}$$

$$= \frac{3.2 \times 10^4 - 0.02 s}{s^2 + 2.4 \times 10^5 s + 1.6 \times 10^7}$$

Using partial fraction expansion, we get

$$I(s) = \frac{0.1334}{(s + 66.7)} - \frac{0.1534}{(s + 2.4 \times 10^5)}$$

In time domain,

$$i(t) = 0.1334 \cdot e^{-66.7t} - 0.1534 \cdot e^{-2.4 \times 10^5 t}$$

The initial current: substitute $t=0$;
 $i(0) = 0.1334 - 0.1534 = 20 \text{ mA}$.

The at which current crosses the zero axis:

$$0.1334 \cdot e^{-66.7t} - 0.1534 \cdot e^{-2.4 \times 10^5 t} = 0$$

$$0.1334 \cdot e^{-66.7t} = 0.1534 \cdot e^{-2.4 \times 10^5 t}$$

Taking log on both sides,

$$\ln(0.1334) - 66.7t = \ln(0.1534) - 2.4 \times 10^5 t$$

$$\text{Thus } t_0 = 0.58 \times 10^{-6} \text{ sec.}$$

Peak value of current:

$$\frac{di}{dt} = 0.1334 \times (-66.7) \cdot e^{-66.7t} - 0.1534 \times (-2.4 \times 10^5) \cdot e^{-2.4 \times 10^5 t} = 0$$

$$8.89778 \times e^{-66.7t} = 36816 \times e^{-2.4 \times 10^5 t}$$

$$-66.7t = \ln\left(\frac{36816}{8.89778}\right) - 2.4 \times 10^5 t$$

$$2.3993 \times 10^5 t = 8.3279$$

$$t = 34.7 \times 10^{-6}$$

Corresponding current would be

$$i(t) = 0.1334 \cdot e^{-66.7 \times 34.7 \times 10^{-6}} - 0.1534 \cdot e^{-2.4 \times 10^5 \times 34.7 \times 10^{-6}}$$

$$= 133 \text{ mA}$$

The steady state value of current is zero.

